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Location-aware ingestible microdevices for wireless monitoring of gastrointestinal dynamics

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Fig. 1: (a) Frequency encoding performed in MRI using hydrogen atoms. (b) Micro-chips working as artificial atoms to perform frequency encoding without any B_0 [13]. (c) Micro-chips localized using magnetic-field gradient encoding, eliminating both B_0 and frequency encoding in this work.



Fig. 2: (a) In vitro localization of a single iMAG with respect to the global origin (0,0,0) of the coils at n=30 different locations chosen uniformly in the FOV. (b) Errors at all 30 locations clustered together. (c) Error at each location is plotted separately. Reported as mean \pm std: 1.07 ± 1.44 mm (X), 0.77 ± 1.07 mm (Y), 1.13 ± 1.20 mm (Z). (d) In vitro localization of iMAG with respect to another iMAG at a known location serving as a relative reference. This eliminates the need for a global reference point. n=30 different locations were chosen uniformly in the FOV. (e), (f) Error in the decoded position of iMAG localized with respect to a reference iMAG. Error as mean \pm std: 1.34 ± 1.68 mm (X), 1.13 ± 1.38 mm (Y), 0.97 ± 1.55 mm (Z).



Fig. 3: (a) A test fixture was prepared with two iMAG devices positioned a fixed distance apart (81.12mm) and lodged into the gastric cavity of the pig via an endoscope. (b) *In vivo* measurement data for three consecutive trials while the fixture is inside the gastric cavity of the pig. The decoded inter-device distance from iMAG is 83.6 ± 0.7 mm (mean \pm std). Individual errors in the X, Y and Z components of the decoded distance are <5mm, the theoretical error-bound of our system. (c) Right, (d) vertical, and (e) left sided X-ray scans of the animal showing the position of the fixture.



Fig. 4: (a) In vivo measurement data when iMAG is located inside the stomach of the pig. The ground truth (24.44cm) is obtained using orthogonal X-rays taken from the (b) right, (c) vertical, and (d) left side of the animal. The decoded distance of iMAG from the external reference iMAG is 24.47 ± 0.12 cm (mean \pm std). Individual errors in the X, Y and Z components of the decoded distance are <5mm, the theoretical error-bound of our system.



Fig. 5: (a) In vivo measurement data when iMAG is located inside the colon of the pig. The ground truth (21.37cm) is obtained using orthogonal X-rays taken from the (b) right, (c) vertical, and (d) left side of the animal. The decoded distance of iMAG from the external reference iMAG is 20.20 ± 0.01 cm (mean \pm std). Individual errors in the X and Y components of the decoded distance are >5mm, which is an artifact caused by the X-ray acquisition methodology, as explained in the Methods section.



Fig. 6: (a) In vivo measurement data when iMAG is located inside the rectum of the pig. The ground truth (20.00cm) is obtained using orthogonal X-rays taken from the (b) right, (c) vertical, and (d) left side of the animal. The decoded distance of iMAG from the external reference iMAG is 19.45 ± 0.40 cm (mean \pm std). Individual errors in the X, Y and Z components of the decoded distance are <5mm, the theoretical error-bound of our system.



Thickness: 2mm



Fig. 7: Complete overview of the printed circuit board (PCB) designed for iMAG. The coin-cell battery is mounted on the side of the antenna and away from the sensor location, to avoid potential interference caused by the weakly magnetic casing of the battery.



Fig. 8: Complete schematic of the iMAG device. All the circuit components and their relative interconnections are shown. The values of the components shown in both the matching networks are tuned in real time to account for the fabrication-related mismatches. The final values used in the two matching networks are shown in Fig. 2c of the main text.



Fig. 9: Matching network tuning performed in real-time using Microwave Vector Network Analyzer (FieldFox) and Spectrum Analyzer. Impedance plot on the Smith Chart with (a) only the FieldFox probe (1.5pF), and (b) FieldFox probe connected to iMAG's RF node ($50\Omega + 1.5pF$). The RF node is shown in Supplementary Fig. 11 (between the two matching networks). Obtaining 50Ω in (b) shows the high accuracy of the matching network used in iMAG.



Fig. 10: Magnetic interference characterization performed by localizing an iMAG device in the presence of magnetic vs non-magnetic beads. (a) iMAG device shown next to highly magnetic barium beads used during the magnetic-label tracking study performed in this work (Fig. 5d-i in main manuscript). (b) Localization error of iMAG plotted vs distance from the barium beads. When the beads are very close to iMAG (<5cm), the error is significantly higher than the 5mm error-threshold of the system due to the distortion caused in the magnetic field by the beads. As the distance of the beads from the iMAG is increased to 10cm or higher, the error falls within the threshold limit which signifies the system's immunity to distortion caused by magnetic objects when located sufficiently away. (c) iMAG device shown next to non-magnetic polyethylene beads used as a negative control to compare against the interference caused by the magnetic barium beads. (d) Localization error of iMAG as the distance of the polyethylene beads is varied from iMAG. As seen, the error values are independent of the proximity from the beads and are within the error-threshold, highlighting the specificity of our system toward magnetic objects.

Z-Actuator Y-Actuator X-Actuator



Fig. 11: Setup for characterizing the magnetic field gradients produced by the coils in the FOV. A 3D magnetic sensor mounted on a wooden arm is moved in the FOV in increments of 1cm in the X, Y and Z directions using three orthogonally connected linear actuators. The magnetic field data measured by the sensor at each step is stored, interpolated (to achieve 1mm resolution), and then used for creating an LUT for position decoding during the localization experiments. More details in [25].



Fig. 12: Design specifications of the wooden chute with adjustable height for the coil-mounting walls.



Fig. 13: Overview of the gradient coil controller circuit. V_{REF} and R_1 together set the value of the DC current since $I_{DC} = V_{REF}/R_1$. An N-channel MOSFET driver M_1 (FDL100N50F) rated for 500V and 100A is used for handling the high DC current coming into the coils. R_1 is chosen with high temperature stability (MP930-0.020-5%) to ensure a thermally stable current value. The coil control is established by the GPIO pins connected to a microcontroller (nRF52DK or Arduino) that serve as the coil enable (ENA) signals.

5	X	Y	Z	B_X	B_Y	BZ	×	X	Y	Z	B _X	$\boldsymbol{B}_{\boldsymbol{Y}}$	BZ
Main Ll	<i>x</i> ₀	${\mathcal Y}_0$	Z ₀	B_{x0}	B_{y0}	B _{z0}	5	<i>x</i> ₂	<i>y</i> ₂	<i>Z</i> ₂	B_{x2}	B_{y2}	B_{z2}
	<i>x</i> ₁	<i>y</i> ₁	<i>Z</i> ₁	B_{x1}	B_{y1}	B _{z1}		<i>x</i> ₅	<i>y</i> ₅	Z_5	B_{x5}	B_{y5}	B_{z5}
	<i>x</i> ₂	<i>y</i> ₂	<i>Z</i> ₂	B_{x2}	B_{y2}	B _{z2}	$\xrightarrow{2}$	<i>x</i> ₂₁	<i>y</i> ₂₁	<i>z</i> ₂₁	<i>B</i> _{<i>x</i>21}	B_{y21}	<i>B</i> _{<i>z</i>21}
$\xrightarrow{1}$	<i>x</i> ₃	<i>y</i> ₃	<i>Z</i> 3	B_{x3}	B_{y3}	B_{z3}		x ₇₈	y ₇₈	Z ₇₈	<i>B</i> _{<i>x</i>78}	B _{y78}	B_{z78}
	<i>x</i> ₄	<i>y</i> ₄	Z_4	B_{x4}	B_{y4}	B_{z4}		<i>x</i> ₅₆₇	y ₅₆₇	Z ₅₆₇	B_{x567}	B_{y567}	B_{z567}
								<i>x</i> ₁₀₅₀	y_{1050}	<i>z</i> ₁₀₅₀	B_{x1050}	B_{y1050}	B_{z1050}
								3					
									-			-	
	x _n	Уn	Zn	B _{xn}	B _{yn}	B _{zn}	ž	Х	Y	Z	B _X	B _Y	BZ
	x _n	<i>Y</i> _n	Z _n	B _{xn}	B _{yn}	B _{zn}	-UT-Y	X <i>x</i> ₂₁	Y <i>y</i> ₂₁	Z z ₂₁	B_X B_{x21}	В _Y В _{y21}	B _Z B _{z21}
Inpu	x_n at - B_{xi} ,	y_n B_{yi}, B_{zi}	Z_n i B \cdot in M	B_{xn} Outj	B_{yn} put - x_i ,	B_{zn} y_i, z_i	LUT-Y	X x ₂₁ x ₅₆₇	Ү У21 У567	Z Z ₂₁ Z ₅₆₇	B_X B_{x21} B_{x567}	В _Y В _{у21} В _{у567}	B _Z B _{z21} B _{z567}
Inpu Step LUT	x_n at - B_{xi} , b 1 - Sea C -X with	y_n B_{yi}, B_{zi} arch for all value	z_n B_{xi} in Massian Mathematical Structures within the second structure of the second structure	B_{xn} Outj Iain LU' n ± ΔB .	B_{yn} put - x_i , Γ and cr	B_{zn} y_i, z_i eate	LUT-Y	X x ₂₁ x ₅₆₇ x ₁₀₅₀	Y <i>Y</i> 21 <i>Y</i> 567 <i>Y</i> 1050	Z Z ₂₁ Z ₅₆₇ Z ₁₀₅₀	B_X B_{x21} B_{x567} B_{x1050}	B _Y B _{y21} B _{y567} B _{y1050}	B_Z B_{Z21} B_{Z567} B_{Z1050}
Inpu Step LUT Step	x_n at - B_{xi} , b 1 - Sea c -X with b 2 - Sea	y_n B_{yi}, B_{zi} arch for z_i all valu	z_n B_{xi} in M les withi B_{yi} in L	B_{xn} Outj Iain LU' n $\pm \Delta B$. UT-X au	B_{yn} put - x_i , T and cr and create	B_{zn} y_i, z_i eate	LUT-Y	X x ₂₁ x ₅₆₇ x ₁₀₅₀	Y <i>Y</i> 21 <i>Y</i> 567 <i>Y</i> 1050	Z Z ₂₁ Z ₅₆₇ Z ₁₀₅₀	B _X B _{x21} B _{x567} B _{x1050}	В _Y В _{y21} В _{y567} В _{y1050}	B _Z B _{z21} B _{z567} B _{z1050}
Inpu Step LUT Step LUT	x_n at - B_{xi} , b 1 - Sea b - X with b 2 - Sea c - Y with	y_n B_{yi}, B_{zi} arch for all value arch for all value all value	z_n B_{xi} in N_{xi} B_{yi} in L es withi B_{yi} in L	B_{xn} Outj Iain LU' n $\pm \Delta B$. UT-X an n $\pm \Delta B$.	B_{yn} put - x_i , T and cr and create	B _{zn} y _i , z _i eate	-Z LUT-Y	X x ₂₁ x ₅₆₇ x ₁₀₅₀	Y <i>Y</i> 21 <i>Y</i> 567 <i>Y</i> 1050	Z Z ₂₁ Z ₅₆₇ Z ₁₀₅₀ 4	B _X B _{x21} B _{x567} B _{x1050}	B _Y B _{y21} B _{y567} B _{y1050}	B _Z B _{Z21} B _{Z567} B _{Z1050}
Inpu Step LUT Step LUT Step	x_n 1 - Sea -X with 2 - Sea -Y with 3 - Sea -7 with	y_n B_{yi}, B_{zi} arch for all value all value arch for all value arch for all value	z_n B_{xi} in M_{zi} B_{yi} in L_{zi} B_{zi} in L_{zi} B_{zi} in L_{zi}	B_{xn} Iain LU' Iain LU' In $\pm \Delta B$. UT-X au In $\pm \Delta B$. UT-Y ar In $\pm \Delta P$	B_{yn} put - x_i , T and cr and create	B_{zn} y_i, z_i eate	UT-Z LUT-Y	X x ₂₁ x ₅₆₇ x ₁₀₅₀	Y <i>Y</i> 21 <i>Y</i> 567 <i>Y</i> 1050 Y	Z Z ₂₁ Z ₅₆₇ Z ₁₀₅₀ 4 Z	B _X B _{x21} B _{x567} B _{x1050} B _X	B _Y B _{y21} B _{y567} B _{y1050}	B _Z B _{Z21} B _{Z567} B _{Z1050}
Inpu Step LUT Step LUT Step LUT	x_n 1 - Sea -X with 2 - Sea -Y with 3 - Sea -Z with	y_n B_{yi}, B_{zi} arch for all value arch for all value arch for all value arch for all value	z_n B_{xi} in M les withi B_{yi} in L es withi B_{zi} in L es withi	B_{xn} Iain LU' n $\pm \Delta B$. UT-X an n $\pm \Delta B$. UT-Y an n $\pm \Delta B$.	B_{yn} put - x_i , T and create and create in LUT	B_{zn} y_i, z_i eate	LUT-Z LUT-Y	X x ₂₁ x ₅₆₇ x ₁₀₅₀ X x ₅₆₇	Y y21 y567 y1050 Y y567	Z Z ₂₁ Z ₅₆₇ Z ₁₀₅₀ 4 Z Z ₅₆₇	B _X B _{x21} B _{x567} B _{x1050} B _X B _X	B _Y B _{y21} B _{y567} B _{y1050} B _Y B _{y567}	Bz Bz21 Bz567 Bz1050 Bz Bz

Fig. 14: Overview of the 3D search algorithm for position decoding from the magnetic field values measured by iMAG. More details in [25].



Fig. 15: (a) iMAG's system-connection procedure for all constituent components. (b) Measurement initiation from the external smartphone. (c) Central client (receiver board) receives the notification from the smartphone and triggers measurements by sending signals to all the connected servers (iMAGs) and enabling the required gradient coil sequence. (d) iMAGs perform all magnetic field and temperature measurements and send them to the central client, which stores all the data in flash memory and prints it out on a computer that it is connected to.

iMAG's Operation Mode	DC/DC Regulator Disabled: Current Consumption	DC/DC Regulator Enabled: Current Consumption
System Off Idle-mode	0.3μΑ	0.3μΑ
System On Idle-mode	10μΑ	8μΑ
Peak Consumption during Advertising	15mA	8mA
Average Consumption during Advertising	440μΑ	230μΑ
Connection Mode Standby	120μΑ	80μΑ
Peak Consumption during I2C Data Transmission	13mA	6mA
Average Consumption during I2C Data Transmission	250μΑ	180μΑ

Table-I: iMAG's Power Consumption Summary

To make the iMAG highly power-efficient, the DC/DC regulator for the NRF BLE chipset is enabled which results in almost 2x power saving (comparing the right two columns in the above table).

Extended Data Fig. 3 Video:

DOI on figshare (https://figshare.com/): 10.6084/m9.figshare.24076089

Extended Data Fig. 4 Video:

DOI on figshare (https://figshare.com/): 10.6084/m9.figshare.24078711